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# Analysis of undulator and gyro-synchrotron radiation for application at tera-hertz

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**Abstract.** We analyze the undulator and gyro -synchrotron radiation of the devices by equating the number of periods of the helical trajectory of the gyrating motion to the number of undulator periods. The gyro radiation is characterized by cyclotron resonance maser interaction exhibits superior line width quality but higher sensitive to beam energy spread when operated at tera-hertz due to finite larmor radius effects.

## 1. Introduction

Over the years the undulator technology have been renewed and upgraded enabling the free electron laser ( FEL) [1-5] to be useful for different physics, chemistry, biology and engineering based applications. The bi-period, staggered array undulator, step tapered, Optical klystron undulators, Apple type and Delta undulators are examples of higher generation FEL schemes. On the other hand, electron cyclotron resonance masers (CRM) have been studied and developed in various schemes [6-10]. The Gyrotrons including Gyro-Klystrons, Gyro-TWTs, Gyro-BWO and Cyclotron Auto Resonance Masers (CARM) work on the principle of electron cyclotron resonance interactions.

Both the free electron laser and electron cyclotron resonance maser share important analogy and similarities [11-14]. The stimulated emission occurs in free electron laser due to ponderomotive wave causing axial micro bunching of electrons along the length of the undulator. The stimulated emission occurs in electron cyclotron maser due to azimuthal bunching of electrons due to relativistic cyclotron frequency. The free electron laser is tuned by varying either the electron beam energy or the undulator magnetic field strength. The wavelength of the electron cyclotron maser radiation is tuned by changing the electron beam energy or the axial magnetic field strength. In CRM, the resonance condition is given by  $\omega = \omega_c + kc\beta_z$ ,  $\omega, k$  are the electromagnetic wave angular frequency & axial wave number respectively.  $\omega_c = eB_0 / \gamma m_e$  is the relativistic cyclotron frequency,  $B_0$  is the axial magnetic field and  $e, m_e$  are the charge of electron and mass respectively. The resonance condition in the case of FEL reads  $\omega = \omega_u + kc\beta_z$ ,  $\omega_u$  is the undulator frequency.  $\beta_z$  is the longitudinal electron velocity.  $\gamma = (1 - \beta_z^2 - \beta_x^2)^{-1/2}$  is the relativistic factor relating to the electron longitudinal velocity and



electron transverse velocity. Substituting the expression for the longitudinal velocity, we get  $\omega = 2\gamma^2\omega_u / 1 + K^2$  for the free electron laser and  $\omega = 2\gamma\omega_c / 1 + \gamma^2\beta_\perp^2$  for the electron cyclotron maser.  $K = 93B_1(T)\lambda_u(m)$  is the undulator parameter relating to the undulator field strength i.e.  $B_1$  and the period length of the undulator  $\lambda_u$ .  $\beta_\perp$  is the initial electron transverse velocity of the gyrating electrons. The radiation frequency scaling with energy is linear i.e.,  $\omega \sim \gamma^1$  in the electron cyclotron resonance maser rather than squared i.e.,  $\omega \sim \gamma^2$  in free electron laser and to make the devices operate differently in tera hertz application [15-24].

In this paper we analyze the undulator radiation and gyro-synchrotron radiation by equating the period of the helical trajectory of the gyro device to the number of undulator periods. In section 2, the undulator radiation is reviewed. In section 3, the expression for the gyro synchrotron radiation is derived and compared. In section 4, results of the analysis are discussed. The effects of the beam energy spread is included in both the devices. It is shown that the gyro device yields comparable photons per second per mrad<sup>2</sup> per 1% bandwidth with undulator based device but with higher sensitive in beam energy spread.

## 2. Undulator radiation

The field of an undulator is denoted as,

$$\vec{B} = [0, \{B_1 \sin(k_u z)\} \hat{y}, 0] \quad (1)$$

Where  $\lambda_u$  is the undulator period with  $k_u = 2\pi/\lambda_u$ .  $\omega_u = ck_u$ .  $B_1$  is the field amplitudes. Using Lorentz force equation we get,

$$\beta_x = -\frac{K}{\gamma} [\cos(k_u z)] + \theta_x \quad (2)$$

Where  $K = eB_1/m_eck_u$  is an undulator parameter. Eq. (2) assumes imperfect trajectory with angular incidence. Further the longitudinal electron velocity as,

$$\beta_z = \beta^* - \frac{K^2}{4\gamma^2} [\cos(2\omega_u t)] + \frac{K\theta_x}{\gamma} [\cos(\omega_u t)] \quad (3)$$

$$\beta^* = 1 - \frac{1}{2\gamma^2} \left\{ 1 + \frac{K^2}{2} + \gamma^2\theta_x^2 \right\}$$

From [2,3], the transverse and the longitudinal electron trajectory is written as,

$$\begin{aligned} x &= -\frac{cK}{\gamma\omega_u} [\sin(\omega_u t)] \\ z &= \beta^* ct - \frac{cK^2}{8\gamma^2\omega_u} [\sin 2\omega_u t] + \frac{c\theta_x K}{\gamma\omega_u} [\sin \omega_u t] \end{aligned} \quad (4)$$

The brightness is calculated with the help of the Lienard-Weichert integral,

$$\frac{d^2I}{d\omega d\Omega} = \frac{e^2\omega^2}{16\pi^3\epsilon_0 c} \left| \int_{-\infty}^{+\infty} \left\{ \hat{n} \times (\hat{n} \times \vec{\beta}) \right\} \exp \left[ i\omega \left( t - \frac{z}{c} \right) \right] dt \right|^2 \quad (5)$$

where,

$$\hat{n} \times (\hat{n} \times \vec{\beta}) \Big|_x = \frac{K}{\gamma} [\cos(k_u z)] - \theta_x \quad (6)$$

The exponential in Eq. (5) reads

$$\exp \left[ i\omega \left( t - \frac{z}{c} \right) \right] = \sum_m J_m(\xi_1, \xi_2) \exp(i\nu_u t) \quad (7)$$

$$\xi_1 = \frac{\omega \theta_x K}{\gamma \omega_u}, \xi_2 = -\frac{\omega K^2}{8\gamma^2 \omega_u}$$

The detuning parameter  $\nu$  is given by

$$\nu_u = \omega_u \left[ \frac{\omega}{2\gamma^2 \omega_u} (1 + K^2/2 + \gamma^2 \theta_x^2) - m \right] \quad (8)$$

Where  $J_m(\xi_1, \xi_2)$  is the Generalized Bessel Functions (GBF)[25]. Using the expressions from above, we get,

$$\frac{d^2 I}{d\omega d\Omega} = \sum_m \frac{e^2 \omega^2 T^2}{64\pi^3 \epsilon_0 c \gamma^2} [JJ]_u^2 \frac{\sin^2(\nu_u T/2)}{(\nu_u T/2)^2} \quad (9)$$

Where,  $[JJ]_u$  reads as,

$$[JJ]_u = \{J_{m+1}(\xi_1, \xi_2) + J_{m-1}(\xi_1, \xi_2)\} - (2\gamma \theta_x / K) J_m(\xi_1, \xi_2) \quad (10)$$

The resonance condition i.e.  $\nu_u = 0$  is obtained as,

$$\omega = 2\gamma^2 m \omega_u / (1 + K^2/2 + \gamma^2 \theta_x^2) \quad (11)$$

The angular energy distribution function is [26],

$$F_m(K, \gamma \theta_x) = m^2 [JJ]_u^2 \frac{K^2}{(1 + K^2/2 + \gamma^2 \theta_x^2)^2} \quad (12)$$

We rewrite Eq. (9) as

$$\frac{d^2 I}{d\omega d\Omega} = \sum_m \frac{e^2 \gamma^2 N_u^2}{4\pi \epsilon_0 c} \frac{K^2}{(1 + K^2/2 + \gamma^2 \theta_x^2)^2} m^2 [JJ]_u^2 \frac{\sin^2(\nu_u T/2)}{(\nu_u T/2)^2} \quad (13)$$

If the number of photons radiated per second with energy  $\hbar\omega/2\pi$  is  $\dot{N}$  then the power radiated is  $P = \dot{N}\hbar\omega/2\pi$ . The result when calculated in terms of  $d\omega/\omega$  read as ,

$$\frac{d^2 \dot{N}}{d\Omega d\omega/\omega} = \sum_m \frac{e^2 \gamma^2 N_u^2}{4\pi \epsilon_0 c} \frac{I_b}{e} \frac{2\pi}{h} \frac{K^2}{(1 + K^2/2 + \gamma^2 \theta_x^2)^2} m^2 [JJ]_u^2 \frac{\sin^2(\nu_u T/2)}{(\nu_u T/2)^2} \quad (14)$$

Where,  $I_b$  =beam current, in units of photons per second per mrad<sup>2</sup> per 0.1% bandwidth, we get

$$\frac{d\dot{N}}{d\Omega} = 1.74 \times 10^{14} \sum_m N_u^2 E^2 I_b \frac{K^2}{(1 + K^2/2 + \gamma^2 \theta_x^2)^2} m^2 [JJ]_u^2 \frac{\sin^2(\nu_u T/2)}{(\nu_u T/2)^2} \quad (15)$$

Eq. (15) is valid for a monoenergetic electron beam, A beam characterized by a finite spread in beam energy induce shift in the resonance frequency and radiation emitted at a given harmonic. From Eq. (11) we read,  $\Delta\omega/\omega = 2\Delta\gamma/\gamma$ . Assuming that the beam has a Gaussian energy distribution in beam

energy spread with r.m.s value  $\sigma_\epsilon$ ,  $f(\epsilon) = \frac{1}{\sqrt{2\pi}\sigma_\epsilon} \exp\left(-\frac{\epsilon^2}{2\sigma_\epsilon^2}\right)$  we find  $\nu \rightarrow \nu_0 + \delta\nu_\epsilon$ ,

$\delta\nu_\varepsilon = 4N_u\pi\varepsilon$ ,  $\varepsilon = (\gamma - \gamma_0)/\gamma_0$ ,  $\gamma_0$  is the resonant energy for which  $\nu_0 = 0$ . After a handful of algebraic steps, we get from Eq.[15]

$$\frac{d\dot{N}}{d\Omega} = 1.74 \times 10^{14} \sum_m N_u^2 E^2 I_b F_m(K, \gamma\theta_x) f(\nu_u, \sigma_\varepsilon) \quad (16)$$

where  $f(\nu_u, \sigma_\varepsilon) = 2 \int_0^1 dt (1-t) \cos(\nu_0 t) \exp\left(\frac{-16\pi^2 N_u^2 \sigma_\varepsilon^2 t^2}{2}\right)$

### 3. Gyro-synchrotron radiation

In an axial magnetic field, the electron velocity and trajectories are

$$\begin{aligned} \beta_x &= -\beta_\perp \cos(\bar{\omega}_c t) + \theta_x \\ \beta_y &= \beta_\perp \sin(\bar{\omega}_c t) \end{aligned} \quad (17)$$

Where,  $\bar{\omega}_c = eB_0/m_e\gamma$ .  $\omega_c = eB_0/m_e$ . We get the longitudinal component as,

$$\beta_z = \beta^* + \theta_x \beta_\perp \cos \bar{\omega}_c t, \quad \beta^* = 1 - \frac{1}{2\gamma^2} \{1 + \gamma^2 \beta_\perp^2 + \gamma^2 \theta_x^2\}$$

and the electron trajectories as,

$$x = -\frac{c\beta_\perp}{\bar{\omega}_c} \sin(\bar{\omega}_c t), \quad y = -\frac{c\beta_\perp}{\bar{\omega}_c} \cos(\bar{\omega}_c t), \quad z = c\beta^* t + (\theta_x c\beta_\perp / \bar{\omega}_c) \sin \bar{\omega}_c t \quad (18)$$

The triple vector products are evaluated as,

$$\begin{aligned} (\hat{n} \times (\hat{n} \times \vec{\beta}))_x &= \beta_\perp \cos(\bar{\omega}_c t) - \theta_x \\ (\hat{n} \times (\hat{n} \times \vec{\beta}))_y &= -\beta_\perp \sin(\bar{\omega}_c t) \\ \frac{\hat{n} \cdot \vec{r}}{c} &= -\frac{\theta_x \beta_\perp}{\bar{\omega}_c} \sin(\bar{\omega}_c t) + \beta^* t \\ \exp[-i\xi_3 \sin \bar{\omega}_c t] &= \sum_n J_n(\xi_3, 0) \exp(-in\bar{\omega}_c t), \quad \xi_3 = \omega\theta_x \beta_\perp / \bar{\omega}_c \end{aligned} \quad (19)$$

For the exponential We get,  $\exp\left[i\omega\left(t - \frac{z}{c}\right)\right] = \sum_n J_n(\xi_3, 0) \exp(iv_c t)$  (20)

The detuning parameter is defined as,

$$\nu_c = \bar{\omega}_c \left[ \frac{\omega}{2\gamma^2 \bar{\omega}_c} (1 + \gamma^2 \beta_\perp^2 + \gamma^2 \theta_x^2) - n \right], \quad (21)$$

Using the earlier equations, we get Eq. (5) as,

$$\frac{d^2 I}{d\omega d\Omega} = \sum_n \frac{e^2 \omega^2 T^2 \beta_\perp^2}{64\pi^3 \varepsilon_0 c} n^2 [JJ]_c^2 \frac{\sin^2(\nu_c T/2)}{(\nu_c T/2)^2} \quad (22)$$

$$\begin{aligned} [JJ]_c &= a_0 + ia_1, \quad a_0 = \{J_{n+1}(\xi_3, 0) + J_{n-1}(\xi_3, 0)\} - 2(\gamma\theta_x / \gamma\beta_\perp) J_n(\xi_3, 0) \\ a_1 &= \{J_{n+1}(\xi_3, 0) - J_{n-1}(\xi_3, 0)\} \quad \text{where} \quad \xi_3 = 2\gamma\theta_x \gamma\beta_\perp / (1 + \gamma^2 \beta_\perp^2 + \gamma^2 \theta_x^2). \quad \text{We re-write Eq.22 as,} \\ \frac{d^2 I}{d\omega d\Omega} &= \sum_n \frac{e^2 \gamma^2 (\bar{\omega}_c T)^2}{4\pi \varepsilon_0 c} \frac{\gamma^2 \beta_\perp^2}{(1 + \gamma^2 \beta_\perp^2 + \gamma^2 \theta_x^2)^2} n^2 [JJ]_c^2 \frac{\sin^2(\nu_c T/2)}{(\nu_c T/2)^2} \end{aligned} \quad (23)$$

Eq. (23) is further simplified to

$$\frac{d\dot{N}}{d\Omega} = 1.74 \times 10^{14} \sum_n N_c^2 E^2 I_b \frac{\beta_{\perp}^2}{(1 + \gamma^2 \beta_{\perp}^2 + \gamma^2 \theta_x^2)^2} n^2 [JJ]_c^2 \frac{\sin^2(v_c T / 2)}{(v_c T / 2)^2} \quad (24)$$

where  $\omega_c = 2\pi c / \Lambda_c$ ,  $N_c \Lambda_c$  is the total interaction length. The angular energy function is calculated as,

$$F_n(\beta_{\perp}, \gamma \theta_x) = \frac{\beta_{\perp}^2}{(1 + \gamma^2 \beta_{\perp}^2 + \gamma^2 \theta_x^2)^2} n^2 [JJ]_c^2 \quad (25)$$

Eq. (25) alternately can be defined as,

$$F_n(\gamma \beta_{\perp}, \gamma \theta_x) = \frac{\gamma^2 \beta_{\perp}^2}{(1 + \gamma^2 \beta_{\perp}^2 + \gamma^2 \theta_x^2)^2} n^2 [JJ]_c^2$$

Eq. (24) is valid for a monoenergetic electron beam, A beam characterized by a finite spread in beam energy induce shift in the resonance frequency and radiation emitted at a given harmonic. From Eq. (11) we read,  $\Delta\omega / \omega = \Delta\gamma / \gamma$ . Assuming that the beam has a Gaussian energy distribution in beam

energy spread with r.m.s value  $\sigma_{\varepsilon}$ ,  $f(\varepsilon) = \frac{1}{\sqrt{2\pi}\sigma_{\varepsilon}} \exp\left(\frac{-\varepsilon}{2\sigma_{\varepsilon}^2}\right)$  we find  $\nu \rightarrow \nu_0 + \delta\nu_{\varepsilon}$ ,

$\delta\nu_{\varepsilon} = 2N_c \pi \varepsilon$ ,  $\varepsilon = (\gamma - \gamma_0) / \gamma_0$ ,  $\gamma_0$  is the resonant energy for which  $\nu_0 = 0$ .

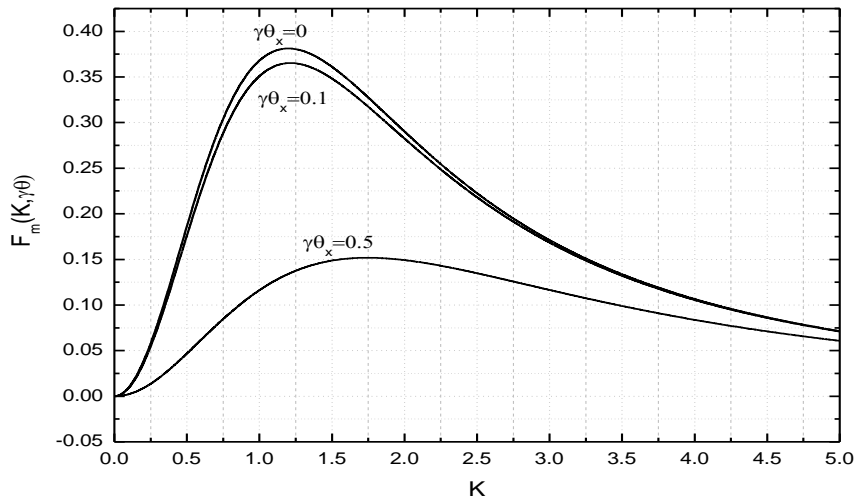
$$\frac{d\dot{N}}{d\Omega} = 1.74 \times 10^{14} \sum_n N_c^2 E^2 I_b F_n(\beta_{\perp}, \gamma \theta_x) f(\nu_c, \sigma_{\varepsilon})$$

Where

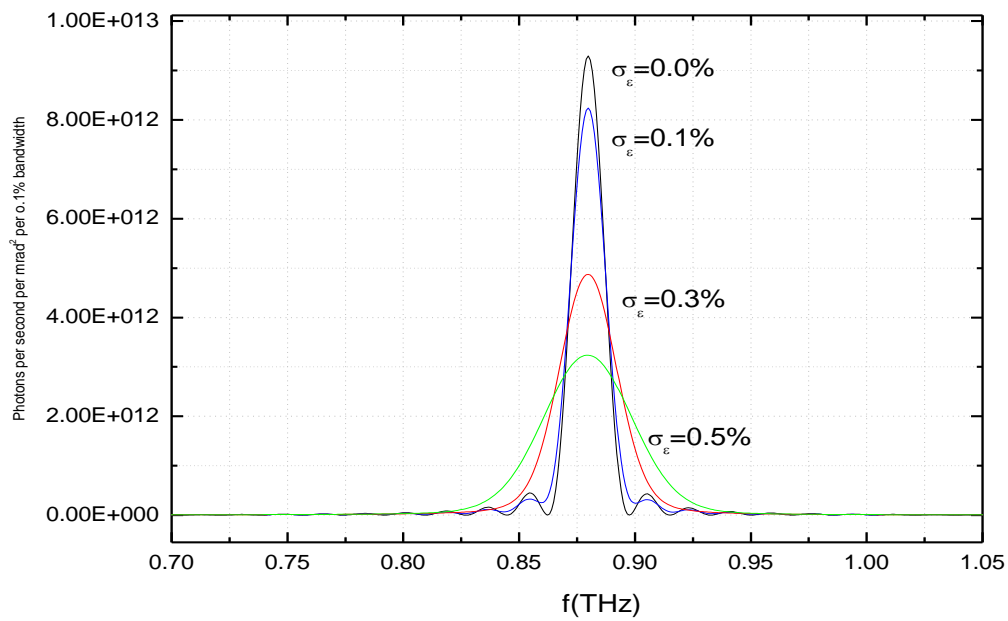
$$f(\nu_c, \sigma_{\varepsilon}) = 2 \int_0^1 dt (1-t) \cos(\nu_0 t) \exp\left(\frac{-16\pi^2 N_c^2 \sigma_{\varepsilon}^2 t^2}{8}\right) \quad (26)$$

#### 4. Results and discussion

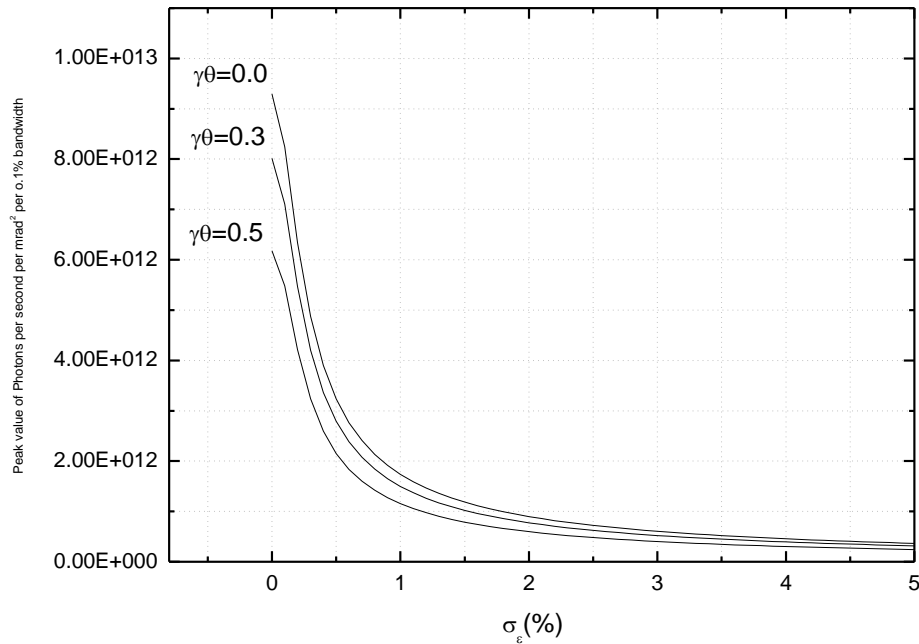
In this paper, we discuss the theory of synchrotron radiation in undulator magnet and compare its characteristics to gyro synchrotron radiation. The electron in the axial magnetic field executes helical trajectories and emits synchrotron radiation at cyclotron resonance frequency. The comparison is based on equating the number of turns in the helical trajectory to the number of undulator periods in the calculations for photons per second per mrad<sup>2</sup> per 0.1% BW. The undulator parameters are  $\gamma = 19.45$ ,  $B_1 = 0.62T$ ,  $K = 2.883$ ,  $N_u = 100$ ,  $\lambda_u = 0.05m$ . The calculations in the paper are done with beam current of 0.3 A. The radiation frequency at these parameters calculates to  $f = 880GHz$ . The angular energy distribution function for the undulator magnet is given in Eq. (12) and is plotted in Figure1. The peak value of this function decreases for higher values of imperfect entry of the electron to the undulator magnet. At  $\gamma\theta_x = 0, 0.1, 0.5$ , the distribution function goes down to 0.36 and 0.15 from 0.38. This amounts to a drop of 5 % and 60 % respectively. The  $\gamma\theta_x = 0.5$  corresponds to 1.5 degree of angular imperfection in the entry of the electron along the undulator magnet. A drop in the value of the distribution function indicates a drop in the photon number. In Figure 2, the effects of beam energy spread on the undulator radiation is shown. A finite beam is characterized by finite energy spread and in our calculation the drop in intensity is about 12 % for  $\sigma_{\varepsilon} = 0.1\%$ . Figure 3 and Figure 4 is plotted for a quantitative evaluation of photons per second per mrad<sup>2</sup> per 0.1% BW at different beam energy spread and angular injection angle of the electron to the undulator magnet.



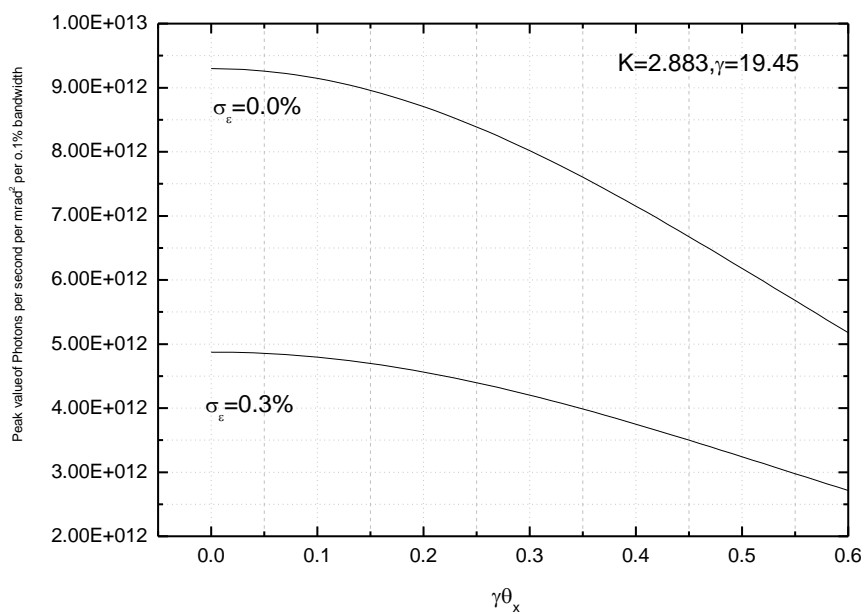
**Figure 1.** Angular energy distribution function of undulator radiation



**Figure 2.** Effects of beam energy spread on photons per second per  $\text{mrad}^2$  per 0.1% BW



**Figure 3.** Effects of beam energy spread

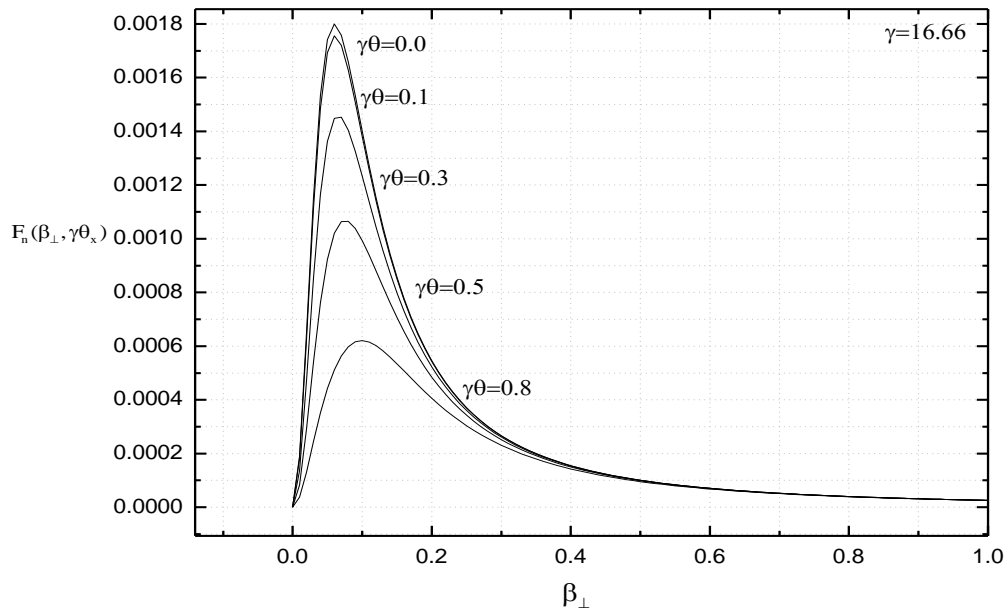


**Figure 4.** Effects of beam energy spread

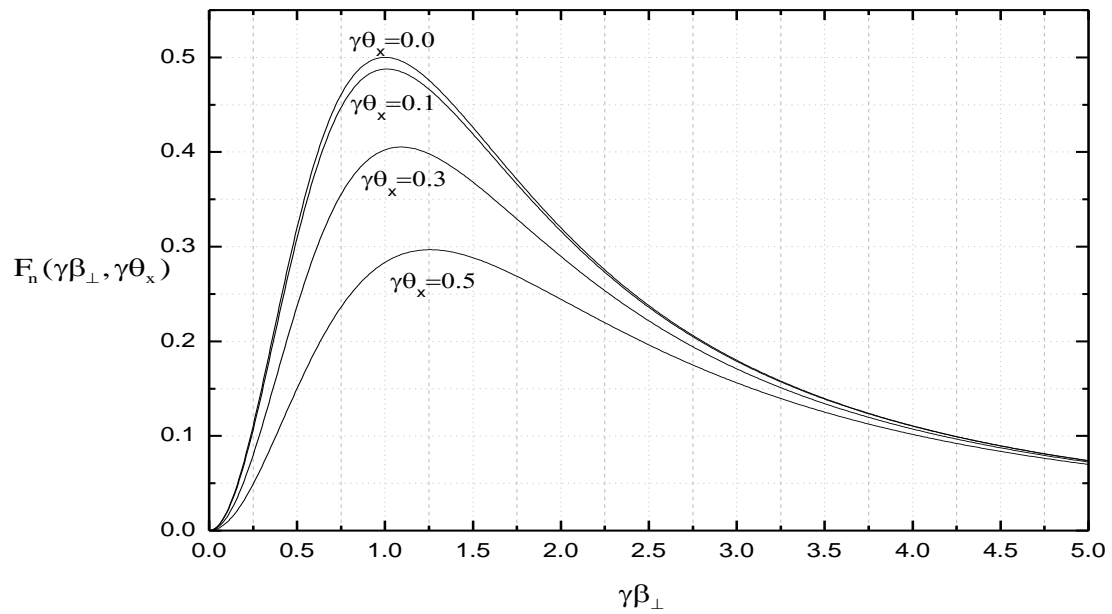
Eq. (25) defines the angular distribution function of the gyro synchrotron radiation and is plotted in Figure 5a and Figure 5b. The function recommends peak value at  $\beta_{\perp} = 0.1$ . The radiation wavelength is fixed 880GHz and equivalent parameter of the gyro synchrotron radiation is calculated



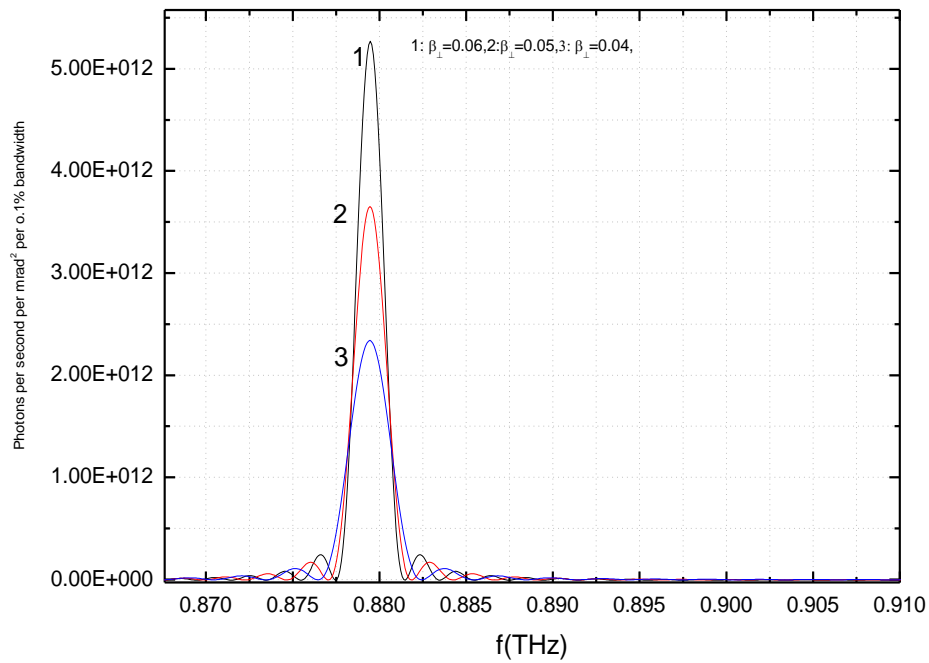
from  $\gamma\beta_{\perp} = 1$  (Figure 5b). The radiation frequency reads from Eq. (21) and is given by  $f = 28\gamma B$  GHz. For parameters of  $\beta_{\perp} = 0.06$ ,  $\gamma = 16.66$ ,  $B_0 = 1.88T$ ,  $f = 880$  GHz, Figure 6 plots photons per second per mrad<sup>2</sup> per 0.1% BW for various values of the beam parameter. By increasing the value of  $\beta_{\perp}$ , the value is increased. The quantity  $\beta_{\perp}$  defines the larmor orbit of the electron i.e  $r_L = c\beta_{\perp} / \omega_c$ . In practical units, using  $f_c = 28B$  GHz we get  $r_L = 1.7 \times 10^{-3} \beta_{\perp} / B$ . For  $\beta_{\perp} = 0.06$ ,  $B_0 = 1.88T$ , the larmor orbit is 54 micron. The larmor orbit is kept at this value in this paper. By decreasing the value of  $\beta_{\perp}$ , the value of the magnetic field requirement is lowered in order that the larmor orbit is kept constant at this value. The photons per second per mrad<sup>2</sup> per 0.1% BW is plotted for several values of  $\beta_{\perp}$  in Figure 6. The corresponding magnetic field requirement is computed from the larmor orbit of 54 micron. At higher  $\beta_{\perp}$ , the intensity is increased can be made comparable to undulator radiation as the radiation is directly proportional to the cyclotron frequency. Higher value of the cyclotron frequency is auto-compulsion in the case as larmor orbit is kept constant. The effect of beam energy spread is studied in Figure 7. The effects of beam energy spread is severe on gyro synchrotron radiation as beam energy spread of 0.1% drops the photons per second per mrad<sup>2</sup> per 0.1% BW by 60%. The reason for this drastic fall is obvious due to following reasons. In order to get a comparable analysis, it is required to keep the interaction length equal. Thus, we are led to  $N_c \Lambda_c = N_u \lambda_u$  where  $N_c, \Lambda_c$  are the number of turns in the helical trajectory and period of the helical trajectory.  $N_u, \lambda_u$  are the undulator number of period and period length respectively  $\Lambda_c = 2\pi c / \omega_c$ . For stronger magnetic field  $\Lambda_c$  is smaller, hence  $N_c$  is higher. For  $\beta_{\perp}$  values of 0.05, 0.06,  $N_c$  is 733 and 880 respectively  $\Lambda_c$  is 6.8 mm and 5.6 mm respectively. Thus, for an undulator length of 50 mm period and 100 periods, the Gyro synchrotron device works as a short period and higher number of period device. This equivalence makes the gyro synchrotron device with comparable intensity with undulator based device but with higher sensitive to beam energy spread.



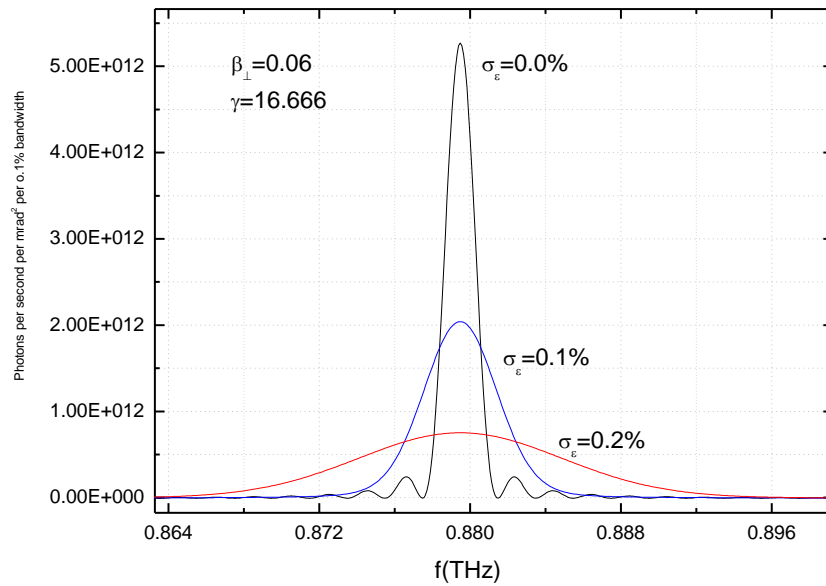
**Figure 5a.** Angular energy distribution function for the gyro radiation



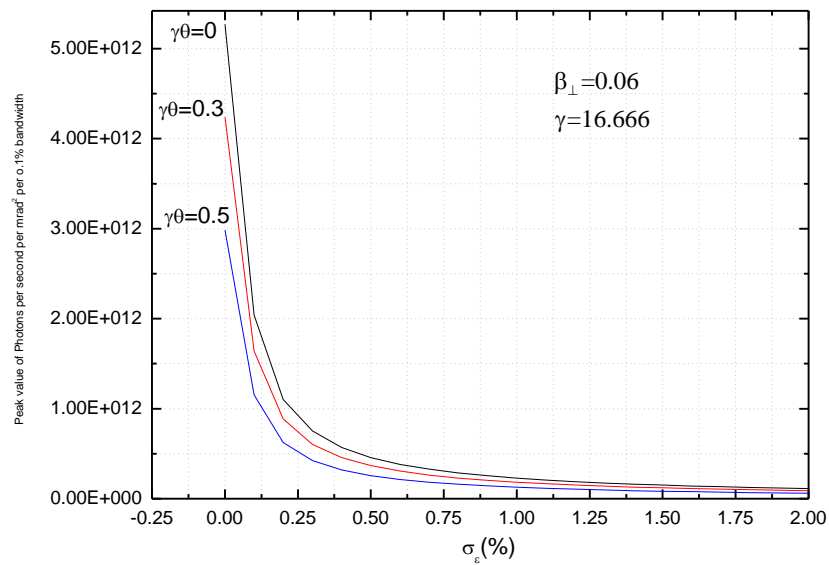
**Figure 5b.** Angular energy distribution function for the gyro radiation



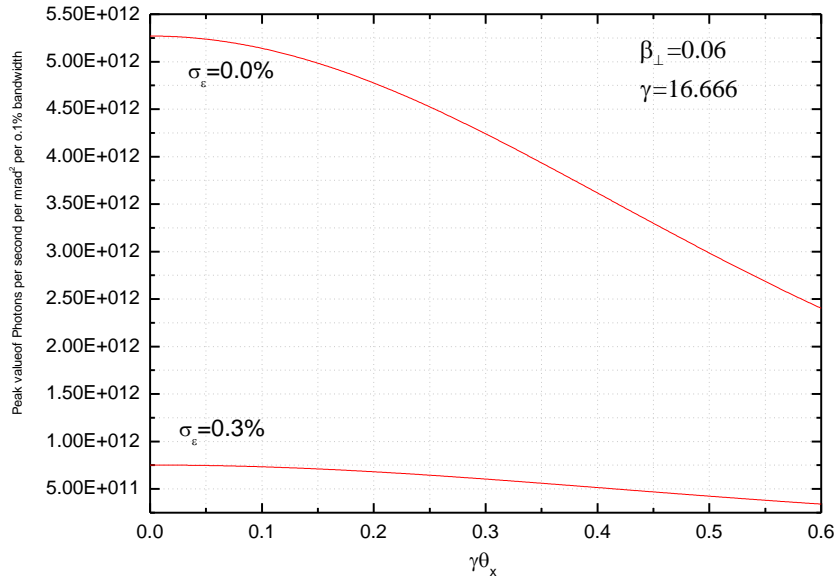
**Figure 6.** Gyro-synchrotron radiation frequency



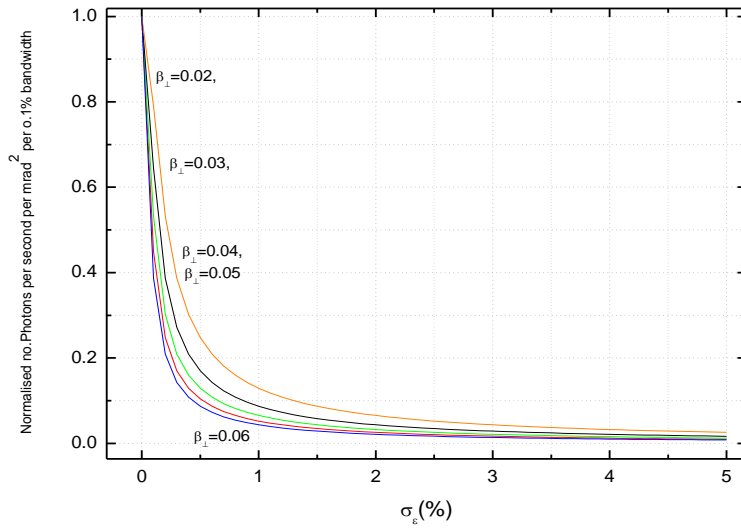
**Figure 7.** Effects of beam energy spread on gyro radiation



**Figure 8.** Effects of beam energy spread and angular injection



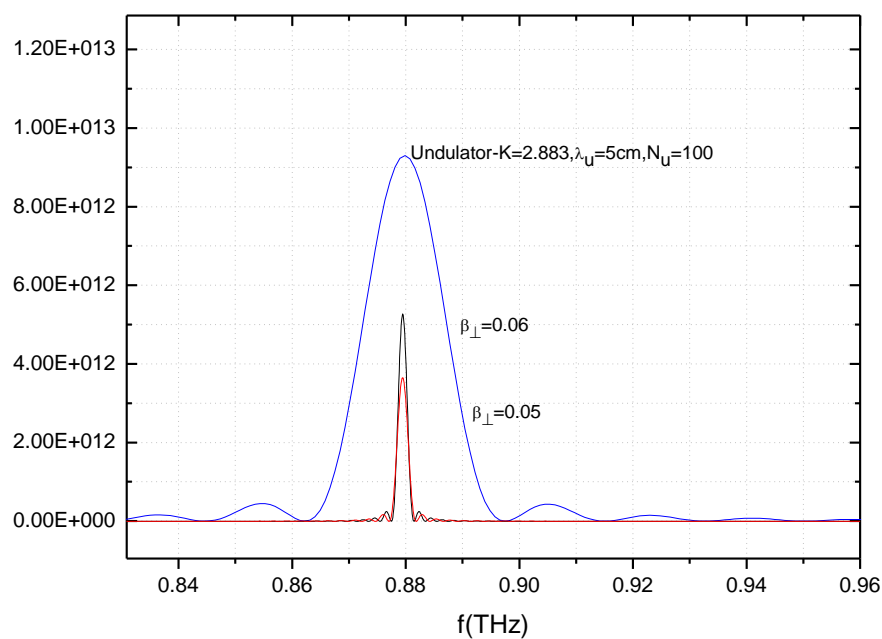
**Figure 9.** Effects of beam energy spread



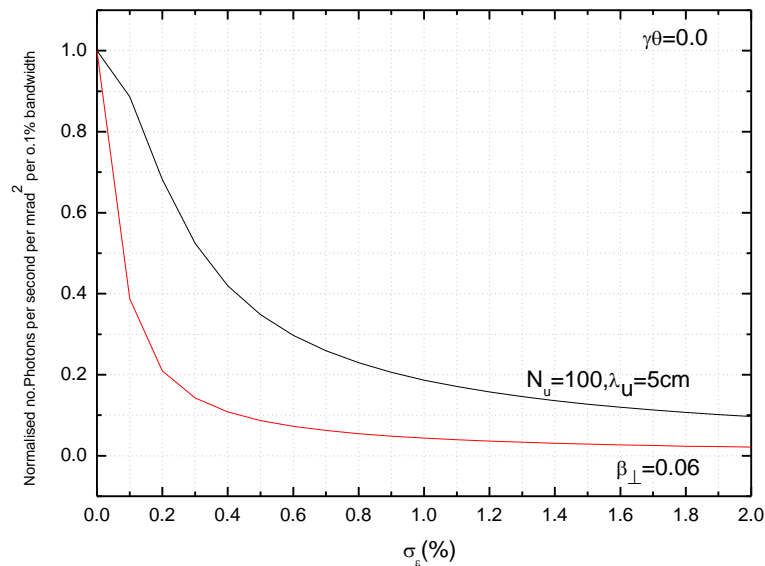
**Figure 10.** Effects of beam energy spread with different  $\beta_{\perp}$

A quantitative evaluation of the beam energy spread with angular effects is given in Figure 8 and Figure 9 respectively. A higher value  $\beta_{\perp}$  is accompanied by higher intensity and carries higher sensitive to beam energy spread due to short period length and higher number of turns as seen in Figure 10. In Figure 11 both the undulator radiation and the gyro radiation are compared. The gyro radiation is superior in terms of the line width over the undulator radiation. The line width of radiation is inversely proportional to the number of periods in undulator based devices. In the calculation the undulator period length is  $\lambda_u = 0.05m$  and number of undulator period is  $N_u = 100$ . In the case with finite  $\beta_{\perp}$ , the period is calculated from  $\Lambda_c = 2\pi c / \omega_c$ . A stronger axial field results in

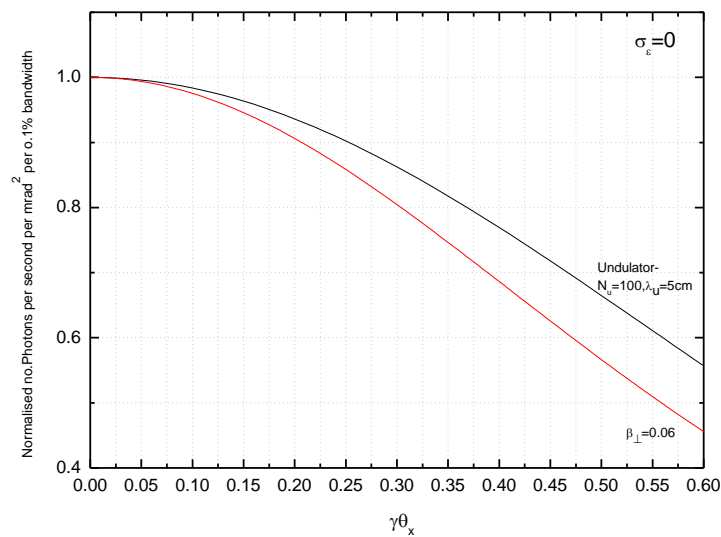
shorter period in comparison to the undulator period, hence more number of periods for the same interaction length and the radiation exhibits good line width behavior shown in Figure 11. In Figure 12 we show the effects of beam energy spread for perfect beam. The gyro radiation has a sharp fall. For a perfect beam the gyro radiation and undulator radiation exhibit less sensitive as compared to imperfect entry, however at large values this effect is substantially large (Figure 13).



**Figure 11.** Line width comparison undulator radiation and gyro radiation



**Figure 12.** Effects of beam energy spread: undulator and gyro device



**Figure 13.** Effects of an angle on undulator and gyro device

In conclusion, the undulator radiation and gyro synchrotron radiation is analyzed with a number of equivalent parameters. The gyro radiation characterized by cyclotron resonance maser interaction exhibits superior line width quality but higher sensitive to beam energy spread when operated at terahertz.

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