

A diagram of the experimental setup is shown in Fig. 1 (a). The experimental setup contains four sections: master laser stabilization, dual timing link stabilization, remote microwave source stabilization, and carrier suppression phase noise measurement. The master laser is a MLL with a pulse duration of 160 fs and pulse repetition rate of 216.667 MHz, which is phase locked to a microwave reference with a locking bandwidth of 10 Hz to enhance its

long-term stability. The optical pulse train emitted from the MLL is split into two parts and then delivered as the timing signal into two independent dispersion compensated polarization maintaining fiber (DC-PMF) links with a length of 1.2 km and 3.5 km, respectively. A fiber-coupled partial reflector at the end of each link provides optical signals for the BOCs in the link inputs upon back-reflection and for the BOMPDs in the link outputs upon transmission. The reflected pulses are combined with new laser pulses in the BOCs to generate error signals for active stabilization of the links to obtain a high precision timing reference at the end of each link. Each transmitted pulse is sent into a BOMPD to phase lock a remote voltage-controlled oscillator (VCO) operating at 10.833 GHz. The microwave signal at the output of each VCO is split into two parts: one part is injected into the BOMPD, and the other part is fed into the out-of-loop carrier suppression noise measurement setup (CS-NMS). Sensitivities of the two BOMPDs at the output of the 1.2 km link and the 3.5 km link are 0.6 mV/fs and 0.2 mV/fs, respectively. We employ free space components to replace fiber components as well as shorten the fiber length of Sagnac interferometers (SGI) in the BOMPDs to optimize the long-term stability. As shown in Fig. 2 (b), optical pulses from the link output are detected by two free-space photodetectors (PD) to generate bias and reference signals divided by the frequency dividers (DIV) for BOMPDs. The generated error signal is sent into a proportional-integral (PI) controller, whose output is feedback to the VCOs to lock them remotely to the master laser. Then, the out-of-loop CS-NMS with noise floor of 69.7  $\mu\text{rad}$  and sensitivity of 23.2 V/rad is used to measure the relative phase error between the two VCOs. In this CS-NMS scheme, attenuator ( $\alpha$ ) and phase shifter ( $\phi$ ) are tuned to minimize amplitude and phase difference between the two microwave signals. A  $180^\circ$  hybrid coupler acts as a microwave interferometer achieving constructive ( $\Sigma$ ) and destructive interference ( $\Delta$ ). The carrier-suppressed signal from the  $\Delta$  output is amplified by a low noise amplifier (G) and converted to a baseband error signal upon mixing with the  $\Sigma$  output. Phase shifter ( $\phi$ ) in one of the arms of the mixer is used to set the two signals in quadrature ensuring pure phase detection.

### 3. Results and Discussion

Relative phase noise and drift between the two synchronized VCOs is measured by the out-of-loop CS-NMS. Fig 2 (a) shows the phase noise spectral density over the frequency range of [1 Hz, 100 MHz]. The accumulated phase error of the system above 1 Hz is only 77.9  $\mu\text{rad}$  for the 10.833 GHz carrier frequency. The pink axis shows the equivalent SSB phase and it exhibits a phase noise of only -108 dBc/Hz at 10-Hz offset from the carrier. Fig. 2 (b) shows phase drift between two remotely synchronized VCOs below 1 Hz. The timing deviation is only 8.85 fs peak-to-peak and 1.76 fs RMS over 2.5 hours of continuous operation. The corresponding maximum phase deviation is about 602.7  $\mu\text{rad}$  and RMS phase drift is 119.6  $\mu\text{rad}$ . These results indicate that the microwave network would enable few-fs level synchronization for radio telescope arrays, next generation accelerator facilities and light sources.

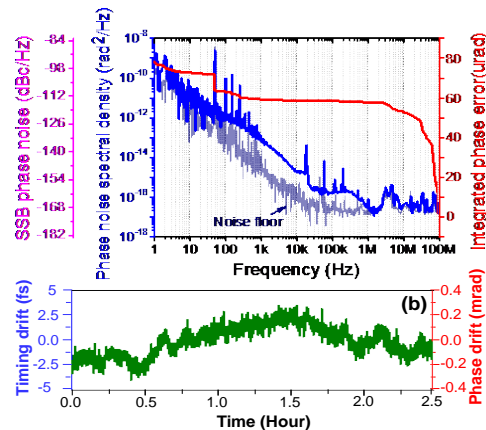


Fig. 2: Out-of-loop measurement results of the microwave network as detected by CS-NMS. (a) Measured phase noise spectral density, its corresponding integrated phase error at 10.833 GHz carrier, and equivalent SSB phase noise; (b) out-of-loop timing and phase drift over 2.5 hours.

### 4. References

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